#### **Supporting Information**

# Digital light processing of 2D lattice composites for tunable self-sensing and mechanical performance

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## **S1. Design of Unit Cells**

Туре	Dimension	$\overline{ ho} = 20\%$	$\overline{ ho} = 30\%$	$\overline{ ho} = 40\%$
	Fillet (R)	0.130	0.195	0.263
	Thickness (t)	0.260	0.390	0.525
hira	Strut length $(l_1)$	1.11	1.05	0.97
0	Strut length $(l_2)$	2.22	2.10	1.94
	Angle $(\theta)$	45°	45°	45°
Ţ.	Fillet ( <i>R</i> )	0.375	0.564	0.750
Hexagona	Thickness (t)	0.375	0.564	0.750
	Strut length (l)	1.35	1.03	0.8
	Angle $(\theta)$	120°	120°	120°
t.	Fillet ( <i>R</i> )	0.225	0.340	0.465
Re-entrar	Thickness (t)	0.225	0.340	0.465
	Strut length (l)	1.4	1.36	1.27
	Angle $(\theta)$	75°	75°	75°
gular	Fillet ( <i>R</i> )	0.045	0.07125	0.095
	Thickness (t)	0.180	0.285	0.380
rian	Strut length (l)	2.57	2.08	1.68
Г	Angle $(\theta)$	60°	60°	60°

Table S1. Dimensions (mm) of different unit cells for each choice of relative density  $\bar{\rho}$ 



Figure S1. Geometrical parameters that define different of unit cell topologies

### **S2.** Microstructure analysis

High-resolution scanning electron microscopy (SEM) was used to analyze the morphology of the as-received MWCNTs. The SEM scans were performed using a scanning electron microscope (Nova NanoSEM 650, FEI Co., USA) with 7.5 kV accelerating voltage and are shown in Fig. S2. It is clear from the images that the MWCNTs are packed into bundles of variable thickness, forming a complex entangled network.



Figure S2. SEM images of the as-received MWCNTs.



## S2. Mechanical behavior of 3D printed MWCNT/Plasclear resin

**Figure S3.** Stress vs. strain (blue) and  $\Delta R / R_0$  vs. strain (red) responses of the 3D printed MWCNT/Plasclear nanocomposite with 0.025 phr MWCNT loading under uniaxial (a) tensile and (b) compressive loading.

Table S2. Measured ultimate strength,	elastic modulus,	failure strain	and gauge	factor of the
3D printed CNT/Plasclear nanocompos	site under uniaxia	al tensile and o	compressiv	e loading.

	Tension	Compression
Elastic Modulus, E(MPa)	$274 \pm 3.17$	$491 \pm 32.5$
Ultimate Strength, $\sigma_u$ (MPa)	$14.8 \pm 0.16$	$46.1 \pm 1.7$
<i>Fracture Strain</i> , $\varepsilon_f(\%)$	14.2 ±0.99	30*
Gauge Factor, k	$1.82\pm0.24^{\dagger}$	$-15.8 \pm 0.55^{\ddagger}$

- $\stackrel{\dagger}{,} 0 \leq \epsilon \leq 4\%$
- $^{\ddagger} 0 \leq \epsilon \leq 4\%$

<sup>\*</sup> Failure strain,  $\epsilon_d$ 

		Ultimate strength, $\sigma^*$				Elastic modulus, E			
		Hexagonal	Chiral	Triangular	Re-entrant	Hexagonal	Chiral	Triangular	Re-entrant
FEA	$\bar{ ho}$ =20%	0.64	0.11	1.11	1.03	11.1	1.13	38.4	32
	$\overline{ ho}$ =30%	1.24	0.27	2.28	1.83	33	3.99	82.6	66.1
	$\overline{ ho}$ =40%	1.99	0.49	2.95	2.83	65.2	10.6	100.7	123.4
Experiment	$\overline{ ho}$ =20%	0.82	0.092	1.38	1.03	13.26	0.898	39.87	33.11
	$\bar{\rho} = 30\%$	1.35	0.33	2.5	1.76	34.1	4.326	71.44	67.04
	$\overline{\rho} = 40\%$	1.98	0.51	3.15	2.82	55.8	13.77	89.18	108.3

**Table S3. Summary of** mechanical properties of 2D cellular structures obtained from experiments and finite element analysis (FEA)

**Table S4. Summary of** scaling parameters of the Gibson-Ashby model obtained from least-square fits to the FE predictions and experimental data, respectively.

		$\log(\overline{\sigma})$				$\log{(\overline{E})}$			
		Hexagonal	Chiral	Triangular	Re-entrant	Hexagonal	Chiral	Triangular	Re-entrant
FEA	y-intercept	-0.244	-0.640	-0.128	-0.165	0.396	-0.148	0.156	0.404
	Slope	1.64	2.16	1.43	1.46	2.56	3.22	1.42	1.94
	Adj. R- Square	0.999	0.999	0.944	0.999	0.998	0.999	0.896	0.994
Experiment	y-intercept	-0.392	-0.438	-0.195	-0.177	0.195	0.374	0.0427	0.199
	Slope	1.27	2.52	1.21	1.44	2.15	4.12	1.26	1.61
	Adj. R- Square	0.999	0.937	0.955	0.993	0.978	0.999	0.991	0.997



**Figure S4.** FE contour plots of the von Mises stress (in MPa) induced in the Chiral lattice structures at various levels of tensile strain; results are presented for three choices of relative density (20%, 30%, and 40%).



**Figure S5.** FE contour plots of the von Mises stress (in MPa) induced in the Re-entrant lattice structures at various levels of tensile strain; results are presented for three choices of relative density (20%, 30%, and 40%).



**Figure S6.** FE contour plots of the von Mises stress (in MPa) induced in the Hexagonal lattice structures at various levels of tensile strain; results are presented for three choices of relative density (20%, 30%, and 40%).



**Figure S7**. FE contour plots of the von Mises stress (in MPa) induced in the Triangular lattice structures at various levels of tensile strain; results are presented for three choices of relative density (20%, 30%, and 40%).