

Impact of stress in ICP-CVD SiN_x passivation films on the leakage current in AlGaIn/GaN HEMTs

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The impact of the stress in room temperature inductively coupled plasma chemical vapour deposited (ICP-CVD) SiN_x surface passivation layers on off-state drain (I_{DS-off}) and gate leakage currents (I_{GS}) in AlGaIn/GaN high electron mobility transistors (HEMTs) is reported. I_{DS-off} and I_{GS} in 2 μm gate length devices were reduced by up to four orders of magnitude to ~ 10 pA/mm using a compressively stressed bilayer SiN_x passivation scheme. In addition, I_{on}/I_{off} of $\sim 10^{11}$ and sub-threshold slope of 68 mV/dec were obtained using this strain engineered surface passivation approach.

Introduction: AlGaIn/GaN HEMTs are a promising candidate for power and RF electronics due to the high breakdown voltage, high electron saturation velocity and good thermal stability of the GaN-based material system [1, 2]. Off-state drain to source (I_{DS-off}) and gate leakage (I_{GS}) currents must be minimised in these devices to improve the efficiency of their power switching. To reduce leakage currents, Al₂O₃ passivation deposited by atomic layer deposition, wet chemical or plasma surface treatment before passivation and annealing after gate metal deposition have been reported [3–6]. SiN_x has been widely used for surface passivation between the transistor gate and drain and shown to be effective in reducing current collapse and DC-to-RF dispersion arising from the large density of surface states and trapped surface charge [7]. Optimisation of the properties of the SiN_x passivation film has been reported, including the impact of stress in the SiN_x film on the properties of an AlGaIn/GaN HEMT by Gregušová *et al.* [8]. Fehlberg *et al.* [9] used Hall Bars to investigate the impact of stress in SiN_x deposited films on the electrical transport properties of AlGaIn/GaN heterostructures. To date, all reports on the impact of stressed SiN_x films have been restricted to passivation layers deposited by plasma enhanced chemical vapour deposition (PE-CVD) techniques with a maximum compressive stress of 150 MPa. Moreover, the use of SiN_x by PE-CVD as a surface passivant can result in increased I_{DS-off} and I_{GS} [10]. To mitigate these effects, in this Letter, we compare the impact of both tensile and compressive stress in the range of -1622 to $+440$ MPa in room temperature deposited ICP-CVD SiN_x surface passivation films on AlGaIn/GaN HEMTs. A significant reduction in I_{DS-off} and I_{GS} was observed for the optimally stressed films.

Fabrication process: The AlGaIn/GaN heterostructure epi-layers of this study were grown on a silicon substrate by metal organic chemical vapour deposition. From the substrate, the layer structure comprised a 0.25 μm AlN nucleation layer; a 10^{18} cm⁻³ carbon doped buffer layer comprising a graded 1.8 μm AlGaIn layer, followed by a 0.8 μm GaN layer; a 0.25 μm undoped GaN channel; a 1 nm mobility enhancing AlN interlayer; a 27 nm Al_{0.27}Ga_{0.73}N barrier and a 2 nm GaN cap layer. Transistors were fabricated by first performing an electron beam evaporation of 30/180/40/100 nm Ti/Al/Ni/Au source and drain ohmic contacts which were annealed at 770°C for 30 s in N₂, followed by a 600 nm mesa isolation etch in a SiCl₄-based plasma chemistry. Then, 2 μm length, 20/200 nm thick Ni/Au Schottky gate contacts were defined by photolithography between the source and drain contacts. At this point, the ‘unpassivated’ transistor characteristics were measured on all samples.

The stress of an ICP-CVD SiN_x passivation film can be adjusted by changing the ICP and RF platen powers [11]. Initially, without any surface pre-treatments, single layers of SiN_x of various stresses were deposited on device samples described above as shown schematically in Fig. 1a. The stress in the films of Table 1 was determined when deposited on silicon substrates. With the exception of films (I) and (V) in Table 1, referred to elsewhere as ‘conventional SiN_x’, all the other films (II to IV of Table 1) cracked or delaminated; an example is shown in Fig. 2a. It was discovered that this situation could be overcome by first depositing 70 nm SiN_x films using process (I) in Table 1 followed by the higher stress films [(II) to (V) of Table 1]. ‘A typical bilayer’ films are shown in Figs. 1b and 2b.

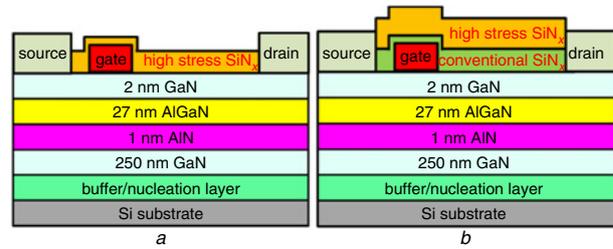


Fig. 1 Cross-section of surface passivation

a ‘High’ stressed single layer surface passivation

b ‘High/conventional’ stressed bilayer surface passivation

Table 1: Stress conditions and type of SiN_x

Ref.	ICP power, W	Platen power, W	Chamber pressure, mT	Stress, MPa	Refractive index
(I)	200	0	5	-280 (compressive)	2.01
(II)	200	4	5	-616 (compressive)	1.99
(III)	300	4	5	-1163 (compressive)	1.93
(IV)	300	8	5	-1622 (compressive)	1.89
(V)	300	0	7	+440 (tensile)	1.72

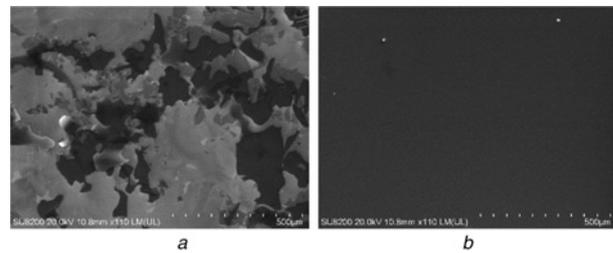


Fig. 2 SEM image of surface passivation

a ‘High’ stressed single layer surface passivation

b ‘High/conventional’ stressed bilayer surface passivation

Measurement results and discussion: Fig. 3 shows room temperature electron mobility (μ_n) and carrier concentration (n_s) as a function of various stress of SiN_x bilayer as determined by Van der Pauw test structure measurement. Electron mobility is increased and carrier concentration is decreased as a consequence of highly compressive stress of SiN_x. This suggests either highly compressive stress of SiN_x passivation schemes have reduction of net positive charge effect at the GaN surface and/or the presence of fixed positive charge in the SiN_x films [12].

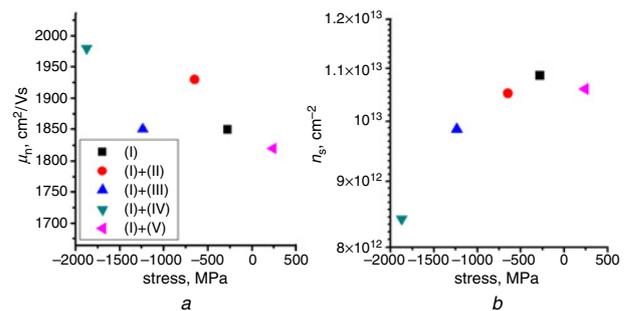


Fig. 3 Room temperature Van der Pauw evaluation

a Stress–electron mobility by various passivation schemes

b Stress–carrier concentration by various passivation schemes

Fig. 4a shows semi-log scale I_{DS-off} – V_{GS} and I_{GS} – V_{GS} characteristics for the single and bilayer passivation schemes and are compared with unpassivated devices. The incorporation of passivations (I) + (II) and (I) + (V) result in three orders of magnitude increase in I_{DS-off} and I_{GS} , when compared to unpassivated devices which have leakage currents of order 10 nA/mm. In contrast, devices with passivation (I) + (IV) have around four orders of magnitude reduction in I_{DS-off} and I_{GS} , when compared to unpassivated devices. Devices with passivation (I) + (IV) demonstrated I_{on}/I_{off} ratio of $\sim 10^{11}$ and subthreshold slope of 68 mV/dec. Fig. 4b shows reverse Schottky gate leakage comparison

of unpassivated and various stressed SiN_x surface passivation schemes. The rank of Schottky reverse bias leakage is same as I_{GS} leakage of Fig. 4a. Figs. 5a and b, respectively, show the $I_{\text{DS}}-V_{\text{DS}}$ three terminal off-state leakage current and $I_{\text{GS}}-V_{\text{DS}}$ lateral isolated leakage current (I_{buffer}) characteristics for the various passivation schemes. These clearly show the bilayer passivation (I)+(IV) is optimal in reducing these contributors to device leakage current.

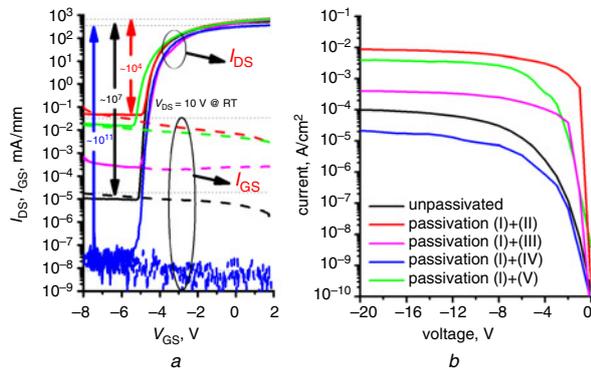


Fig. 4 Semi-log scale off-state and gate leakage comparison of unpassivated and various stressed SiN_x surface passivation schemes

a $I_{\text{DS}}-V_{\text{GS}}$ and $I_{\text{GS}}-V_{\text{GS}}$ comparison ($W_{\text{G}} = 100 \mu\text{m}$, $L_{\text{GS}} = 2 \mu\text{m}$, $L_{\text{G}} = 2 \mu\text{m}$, $L_{\text{GD}} = 7 \mu\text{m}$)
 b Reverse Schottky gate leakage comparison

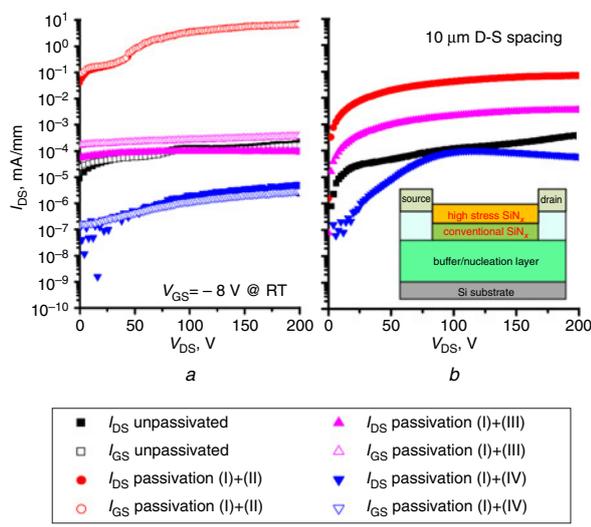


Fig. 5 Semi-log scale off-state and lateral isolated leakage comparison of unpassivated and various stressed SiN_x surface passivation schemes

a $I_{\text{DS}}-V_{\text{DS}}$ and $I_{\text{GS}}-V_{\text{DS}}$ off-state leakage current characteristics ($W_{\text{G}} = 100 \mu\text{m}$, $L_{\text{GS}} = 2 \mu\text{m}$, $L_{\text{G}} = 2 \mu\text{m}$, $L_{\text{GD}} = 7 \mu\text{m}$)
 b Lateral isolated leakage current characteristics

Conclusion: In this Letter, the impact of stress in ICP-CVD SiN_x surface passivation layers deposited at room temperature on $I_{\text{DS-off}}$ and I_{GS} in AlGaIn/GaN HEMTs is assessed. The use of a bilayer SiN_x passivation scheme comprising 70 nm 280 MPa compressively strained film followed by a 150 nm 1.6 GPa compressively strained layer resulted in $I_{\text{DS-off}}$ and I_{GS} reduction by up to four orders of magnitude when compared to unpassivated devices and up to seven orders of magnitude in comparison with devices with a single 70 nm 280 MPa compressively strained passivation layer. $I_{\text{DS-off}}$ and I_{GS} of $\sim 10 \text{ pA/mm}$, $I_{\text{on}}/I_{\text{off}}$ of $\sim 10^{11}$ and subthreshold slope of 68 mV/dec are obtained using the optimal process.

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One or more of the Figures in this Letter are available in colour online.

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